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Analysis of Pile Foundation Bearing Capacity and Soil Classification in Padang City

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Abstract— Padang City, west of Sumatra, is highly vulnerable to natural disasters such as earthquakes, landslides, and floods. The soil conditions in this area, consisting of tuff, silica, and rocks with low cohesion, pose challenges due to their weak bearing capacity, increasing the risk of ground movement or subsidence. This study analyzes the bearing capacity of pile foundations and soil classification in the Sungai Sapih area using the Cone Penetration Test (CPT) method and soil classification based on the Bagemann method. Investigations were conducted at five sounding points (S1-S5) in Sungai Sapih to understand the soil characteristics and provide optimal foundation planning recommendations. The results of this study indicate that the soil layers are dominated by clay, with variations such as organic clay, very stiff clay, and clay loam, all of which tend to have low end-bearing capacity. At depths of up to 11 meters, the cone resistance (qc) values were very low at all points, indicating that the pile foundation cannot rely on end-bearing support at this depth. However, increased friction along the pile shaft significantly contributes to the ultimate bearing capacity of the pile foundation. Hard soil layers were identified at depths of 12-16 meters, with qc values of approximately 150 kg/cm², providing a reference for deep foundation design. Based on the result of this study, the use of piles foundation and bored piles is recommended to reach the hard soil layers to ensure structural stability. Additionally, an analysis of soil settlement is necessary due to the high potential for deformation in the clay layers. This study is expected to serve as a guideline for safe and sustainable foundation planning in the Sungai Sapih area, rapidly developing as a center for government and public facilities in Padang City.

Keywords— Bearing capacity; pile foundation; soil classification.

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I. INTRODUCTION

Padang City is an area that is prone to various natural disasters, such as earthquakes, landslides and floods. [1],[2],[3] Geographically, Padang City is located on the west coast of Sumatra Island. According to Adrin Tohari, Padang City composed of 4 (four) rock layers, consisting of sedimentary rock, volcanic rock and sedimentary rock [4], the type of soil in this area contains tufa, silica and bolder with relatively low cohesion, so it is easily separated when exposed to water. This type of soil does not have a good bearing capacity, so there is a risk of causing ground movement or subsidence if it is not calculated properly. Soil carrying capacity and soil type play an important role in development planning and regional development in the city of Padang. Soil bearing capacity can be determined based on investigations

(soil investigations) based on laboratory data and field data. The most common field investigations carried out on building construction projects, roads, bridges and other public facilities are the Cone Penetration Test (CPT) which is also called the sondir test.

This paper discusses the bearing capacity of pile foundations based on the Cone Penetration Test (CPT) and soil classification using the Bagemann method, conducted in the Sungai Sapih area, Padang City. Given the rapid development in this area, with numerous government centers and public facilities being constructed, a study on soil conditions and bearing capacity is necessary as a foundation for proper planning. This information is essential to provide guidance for the community and local government in supporting safe and sustainable development In civil building construction planning, the bearing capacity of the soil has a very important role. The bearing capacity of the soil is the

ability of the soil to withstand the foundation load without collapsing due to shear which is also determined by the shear strength of the soil. Soil has the property of increasing its density and shear strength when subjected to pressure. If the load acting on the foundation soil has exceeded its limit bearing capacity, the shear stress generated in the foundation soil exceeds the shear strength of the soil, which will result in shear failure of the soil [5],[6].

Ultimate bearing capacity (Qult) is the maximum pressure that can be accepted by the soil to withstand a load without causing landslides or a failure under and around the foundation [7]

The bearing capacity of shallow deep foundations and the bearing capacity of deep foundations are carried out based on static methods using the Terzaghi method (1943). to calculate the end bearing capacity (Qp) and friction bearing capacity (Qs). Carrying capacity analysis can be carried out based on field test results from Standard Penetration Test (SPT) [8] and Cone Penetration Test (CPT) testing [9]

The CPT test, also known as the static cone penetration test, is widely used in Indonesia. This test is a test used to calculate the bearing capacity of the soil. The values of static cone resistance or cone resistance (qc) and adhesive resistance (fs) are obtained from tests and can be directly correlated with the soil bearing capacity [10]. The value of (qc) and (fs) can also indicate the identification of the type of soil and its consistency. In sandy soil, the qc value is greater than in fine-grained soil. In dense and very dense sand, light sondir generally cannot penetrate this layer [11], [12]. The comparison of the amount of resistance fs and qc, known as the friction ratio (Rf), can be used to determine soil classification [13]. Several research results show that coarse-grained soils have a small Rf value (<2%), while for fine-grained soils (silt and clay) the Rf value is higher [14], [13]

II. MATERIALS AND METHOD

A. Soil Classification based on CPT

Bagemann developed soil classification based on CPT data in 1965. There is a correlation between sleeve friction and cone resistance [15].

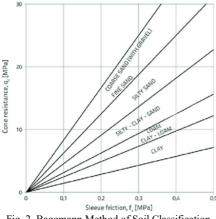


Fig. 2 Bagemann Method of Soil Classification

B. Soil bearing capacity based on CPT Test for Pile Foundations

The bearing capacity of piles can be obtained from CPT or cone penetration test (CPT) data. The mobilized end

resistance of the pile must be equivalent to the end resistance during the penetration test. Hardiyatmo (2001) suggests that for closed-end piles, the unit end resistance of the pile is equal to the cone resistance (qc). However, for open-end piles or bored piles, the unit end resistance is taken as 70% of the cone resistance [16]. The ultimate net bearing capacity (Qu) is calculated using the general equation with,

$$Qu = Qb + Qs = Ab. qc + As.fs$$
 (1)

Ab: area of the pile base, as: surface area of the pile shaft, qc: unit end resistance of the pile, fs: unit skin friction resistance of the pile,

Wp: weight of the pile. states that the load-bearing capacity of the pile foundation is a combination of end resistance and friction [8],[14]

$$Q_u = Q_b + Q_s \tag{2}$$

$$Q_b = \omega . A_b . q_c \tag{3}$$

$$O_s = \Sigma (A_s, q_f)$$
(4)

Qu: ultimate bearing capacity, Qb: end bearing capacity, Qs: friction bearing capacity, ω : reduction factor for nominal end resistance, Ab: cross-sectional area of the pile base (m²), qc: average cone resistance value calculated from 8D above the pile base to 4D below the pile base, As: surface area of the pile shaft, qf: average value of the shaft resistance (kN/m²).

C. Pile Capacity in Granular Soil

Involves using a standard cone penetrometer to measure soil resistance in the Sungai Sapih Area, with multiple tests at each site to ensure reliability.

Soil bearing capacity will be calculated using the relationships for undrained cohesion and ultimate bearing capacity. Statistical analysis will summarize the data and identify relationships between soil parameters.

Results from CPT and soil analysis will offer insights into soil load-bearing capacity, validated against existing literature and standards. The findings will be compiled into a comprehensive report, discussing methodologies, detailed results, and implications for civil engineering practices in Padang City. This research aims to provide critical information for safe and effective construction practices.

The CPT data was obtained from secondary sources related to building construction in the Sungai Sapih area, Aia Pacah, Kota Padang, covering five test points. Bearing capacity analysis was conducted using the Bagemann method, with soil classification also based on the same approach. Table 1 presents the results of the CPT tests at the five locations in Sungai Sapih, Kota Padang. The data provides an overview of the soil conditions at the site, including soil layer depth and parameters such as cone resistance (qc) and friction resistance (qs), which are essential for determining the foundation's bearing capacity. Based on the analysis results, each test point indicates variations in soil consistency and type, serving as the foundation for planning and selecting the optimal foundation type for construction in the area.

As shown in Table 1, the depth of the hard soil layer at the five test points ranges from 12.6 meters to 15.6 meters. Hard soil is generally defined as soil with a high cone resistance value, specifically qc \geq 150 kg/cm². At all test points (S1 to S5), this qc value has been reached, indicating hat a load-

bearing layer exists at these depths capable of supporting the structural load.

D. Analysis of the Bearing Capacity of Pile Foundations

The pile foundation depth is planned with variations of 3 m, 6 m, 9 m, and 12.6 m. The piles used are circular concrete piles with a diameter of 40 cm. The analysis of pile foundation bearing capacity is carried out using the Bagemann method. This calculation is based on CPT test results with the Bagemann method, where the reduction factor for the nominal end resistance value (ω) is 0.50.

The ultimate bearing capacity equation for pile foundation is expressed as:

 $Q_u = Q_b + Q_s$

With,

 $\begin{array}{l} Qu: Ultimit \ bearing \ capacity, \ Q_b \ : \omega.A_b.q_c, \\ Q_s \ : \Sigma \ (\ A_s. \ q_f \) \end{array}$

E. Bearing Capacity of Pile Foundations Calculation (S1)

Foundation Depth: 3 meters, End Bearing Capacity (Qb), Foundation Depth: 3 meters

- End Bearing Capacity (Q_b) Cross-Sectional Area of Pile Tip (A_b): 0.126 m² Avarage of qc (8D-4D): 210,292 kN/m² $Q_b = \omega .A_b.q_c = 0,5^* 0,1256 m^2 * 210,292 kN/m^2 = 13,206 kN$
- Friction Capacity (Qs) Surface Area of the Pile Shaft (As): 3,768 m², Average (qs): 3,267 kN/m² Q_s = Q_s = Σ (A_s. q_f) = Σ(3,768 m²*3,267 kN/m² =
 - $Q_s Q_s 2$ (A_s, q_f) 2(5,768 m⁻¹5,267 kW/m² 12,309 kN
- Ultimate Bearing Capacity (Qu): $Q_u = Q_b + Q_s = 13,206 \text{ kN} + 12,309 \text{ kN} = 25,515 \text{ Kn}$

F. Soil classification by Bagemann Method

The soil classification of the CPT test results is obtained from the Bagemann graph (figure 2), which shows a correlation between sleeve friction and cone resistance

The analysis results of the bearing capacity at each CPT test and soil classification from S1 to S5 (Figures 3 to 12),

• Analysis (CPT Point 1 / S1)

TABLE I Maximum end resistance value (QC)			
No	Location	Dept (m)	Cone Resiatance (qc) (kg/cm ²)
1	S1	12,6	150
2	S2	13,4	150
3	S3	13	150
4	S4	15,6	150
5	S5	14,8	150

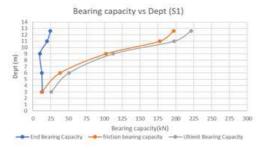


Fig. 3 Foundation bearing capacity at point S1

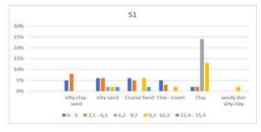


Fig. 4 Soil classification at point S1

• Analysis (CPT Point 2 / S2)



Fig. 5 Foundation bearing capacity at point S2

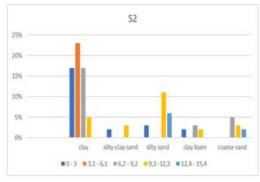


Fig. 6 Soil classification at point S2

• Analysis (CPT Point 3 / S3)

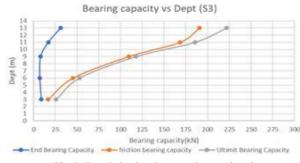


Fig. 7 Foundation bearing capacity at point S3

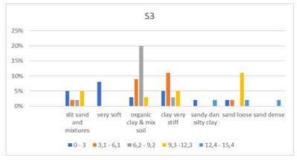


Fig. 8 Soil classification at point S3

• Analysis (CPT Point 4 / S4)



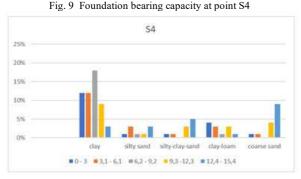
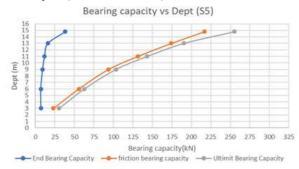
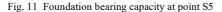


Fig. 10 Soil classification at point S4

• Analysis (CPT Point 5 / S5)





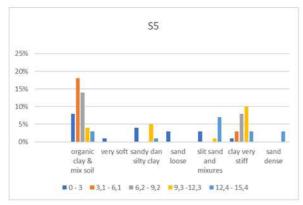


Fig. 12 Soil classification at point S5

III. RESULTS AND DISCUSSION

A. CPT Point 1 (S1)

Soil Bearing Capacity (Figure 3). At depths of 0-9 meters, the end-bearing capacity of the pile is relatively low. However, the increasing frictional resistance with depth indicates that the foundation relies more on friction along the

pile surface to support the load. Soil Classification (Figure 4) At depths of 0-9.2 meters, the soil layer is predominantly composed of clay. Clay soils tend to have low end-bearing capacity and significant cohesive properties. This aligns with the observed characteristics, which show low cone tip resistance.

B. CPT Point 2 (S2)

Soil Bearing Capacity (Figure 5). At point S2, from a depth of 0 to 8.6 meters, the cone tip resistance is low, resulting in low end-bearing capacity. However, it starts to increase at depths between 8.8 and 13.4 meters. This condition indicates the soil's limitations in supporting large loads at those depths. Soil Classification (Figure 3). At depths of 0 to 15.4 meters, approximately 62% of the soil composition is clay. This zone has a low potential for supporting pile foundations and is prone to settlement if high loads are applied.

C. CPT Point 3 (S3)

Soft soil is found from a depth of 0 to 11 meters. The low cone tip resistance indicates inadequate bearing capacity, making the use of pile foundations with loads at the tip ineffective. Soil Classification (Figure 5).

The soil composition at this point is also dominated by organic clay and very stiff clay, reinforcing the assumption that the soil is not optimal for supporting large loads. This soil layer carries a high risk of deformation, especially when saturated with water or subjected to heavy loads.

D. CPT Point 4 (S4)

Soil Bearing Capacity (Figure 6). At point S4, the endbearing capacity is low down to a depth of 11 meters. However, friction along the surface of the pile contributes significantly to the total bearing capacity of the foundation. This indicates that at this location, the use of pile foundations will rely more on friction than on end support. Soil Classification (S4). At this location, the soil is predominantly clay, making up 54% of the composition, which results in relatively low bearing capacity.

E. CPT Point 5 (S5)

Soil Bearing Capacity (S5). At point S5, the soil is predominantly clay from a depth of 0 to 13 meters, exhibiting relatively low end-bearing capacity. The clay layer at this depth indicates a low potential for end-bearing capacity and a reliance on frictional support. Soil Classification

The soil at this location is dominated by clay and clay loam, which are types of soil with low bearing capacity.

At the Sungai Sapih area, hard soil is found at depths between 12 to 15 meters across all five borehole points. This indicates that the soil in this location has low bearing capacity, making it unsuitable for supporting large loads unless the foundation is placed down to the hard soil layer. All borehole points show a similar pattern, with clay layers dominating at various depths, exhibiting low end-bearing capacity but significant frictional support [17], [18]

IV. CONCLUSION

Based on the soil classification results using the Bagemann method from five testing points (S1–S5) in the Sungai Sapih area, Aia Pacah, and Padang City, most of the soil layers are

dominated by clay with various compositions and consistencies, such as organic clay, very stiff clay, and clay loam. Clay soils have low bearing capacity and are cohesive, making them inadequate for supporting large loads without special handling.

According to the analysis of pile foundation-bearing capacity for the Sungai Sapih area, foundation planning should prioritize the use of long piles that reach the hard soil layer while considering the contribution of friction to ensure optimal foundation performance. The hard soil layer is located at depths of 12.6 to 15.6 meters, with a cone tip resistance (qc) value of 150 kg/cm². The soil conditions at the testing location are relatively uniform, which will facilitate a more straightforward and predictive foundation planning process.

Deep foundations such as driven piles or bored piles are recommended to ensure that the foundation reaches the hard soil layer and has adequate bearing capacity. Settlement control is necessary due to the susceptibility of clay layers to settlement, requiring close monitoring of changes in soil conditions, particularly in the event of humidity changes.

REFERENCES

- I. Warman and A. Ardila, "Sistem informasi mitigasi rawan bencana kota Padang berbasis web - ArcGIS," *Explore: J. Sist. Inf. Telemat.*, vol. 13, no. 1, p. 38, Jun. 2022, doi: 10.36448/jsit.v13i1.2536.
- [2] S. E. Putri et al., "Kota Padang: Identifikasi potensi bencana banjir dan upaya mitigasi," *J. Ilm. Multidisiplin Nusantara*, vol. 1, no. 3, pp. 116-122, Jul. 2023, doi: 10.59435/jimnu.v1i3.56.
- [3] A. Alfadhlani, P. Fithri, and D. P. Altha, "Evaluasi risiko terhadap potensi gempa bumi dan tsunami di RSUP Dr. M. Djamil Padang," Pros. Semin. Nas. Tek. Ind., p. 2023, 2023.
- [4] A. Tohari and D. D. Wardhana, "Mikrozonasi seismik wilayah kota Padang berdasarkan pengukuran mikrotremor," *RISET Geol. Pertamb.*, vol. 28, no. 2, p. 205, Nov. 2018, doi:10.14203/risetgeotam2018.v28.984.

- [5] K. Adelia et al., "Soil bearing capacity of shallow foundation based on Terzaghi method in Cipatat, West Bandung, West Java," J. Tek. Sipil, vol. 4, no. 1, pp. 17-22, 2020.
- [6] H. K. Piyasawat, "Bearing capacity of shallow foundation on collapsible Khonkaen loess," *Int. J. Geomate*, vol. 20, no. 80, Apr. 2021, doi: 10.21660/2021.80.j2067.
- [7] R. R. Putra, "Relationship between obtained ultimate bearing capacity results based on N-SPT results and static load tests," *Int. J. Geomate*, vol. 19, no. 74, pp. 153-160, Oct. 2020, doi:10.21660/2020.74.60639.
- [8] A. Resi, "Capacity analysis of single pile bearing capacity based on static method and N-SPT test on pile driving analyzer test (case study of PT. Asahi Forge Indonesia Phase II project)," *Neutron*, vol. 18, no. 2, pp. 10-17, Jan. 2019, doi: 10.29138/neutron.v18i2.74.
- [9] B. Setiawan et al., "Estimating bearing capacity using static cone penetration test at Banda Aceh area (northern tip of Sumatra)," *IOP Conf. Ser.: Mater. Sci. Eng.*, vol. 1087, no. 1, p. 012025, Feb. 2021, doi: 10.1088/1757-899X/1087/1/012025.
- [10] Kementerian Pekerjaan Umum dan Perumahan Rakyat, Kumpulan Korelasi Parameter Geoteknik dan Fondasi, 2019, pp. 1-116.
- [11] Badan Standardisasi Nasional, Cara Uji Penetrasi Lapangan dengan Alat Sondir, SNI 2827:2008, 2008, pp. 1-23.
- [12] S. B. Basri, "Current trend of software requirement engineering process in IT small and medium enterprises (SMEs)-A systematic literature review," in *Proc. 13th Int. Conf. Inf. Technol. Asia (CITA)*, 2023, pp. 82-87, doi: 10.1109/CITA58204.2023.10262498.
- [13] A. Apriyono et al., "Soil classification based on cone penetration test (CPT) data in Western Central Java," *AIP Conf. Proc.*, vol. 1941, p. 020004, 2018, doi: 10.1063/1.5028062.
- [14] N. Juliana and Tarbiyatno, "Hubungan daya dukung tanah berdasarkan hasil sondir, SPT dan laboratorium pada rencana pembangunan gedung multi lantai di lokasi Balige," J. Pendidik. Tek. Bangunan Sipil, vol. 5, no. 2, pp. 45-49, 2019.
- [15] R. Yuliet, M. Mera, and K. Hidayat, "Soil classification at Muaro Baru beach of Padang City using CPT data," *E3S Web Conf.*, vol. 331, p. 03005, 2021, doi: 10.1051/e3sconf/202133103005.
- [16] H. C. Hardiyatmo, Analisis dan Perancangan Fondasi, 4th ed. Yogyakarta: Gadjah Mada University Press, 2018.
- [17] A. Jalil et al., "Analisis daya dukung statik fondasi tiang dari data CPT dengan FS = angka keamanan," J. Tek. Sipil, vol. 1, pp. 1-7, 2023.
- [18] D. Xu et al., "Bearing capacity analysis of offshore pipe piles with CPTs by considering uncertainty," *Comput. Geotech.*, vol. 126, p. 103731, Oct. 2020, doi: 10.1016/j.compgeo.2020.103731.